

# Flexible Joint - Test Bench

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# 1 Flexible Joints - Requirements

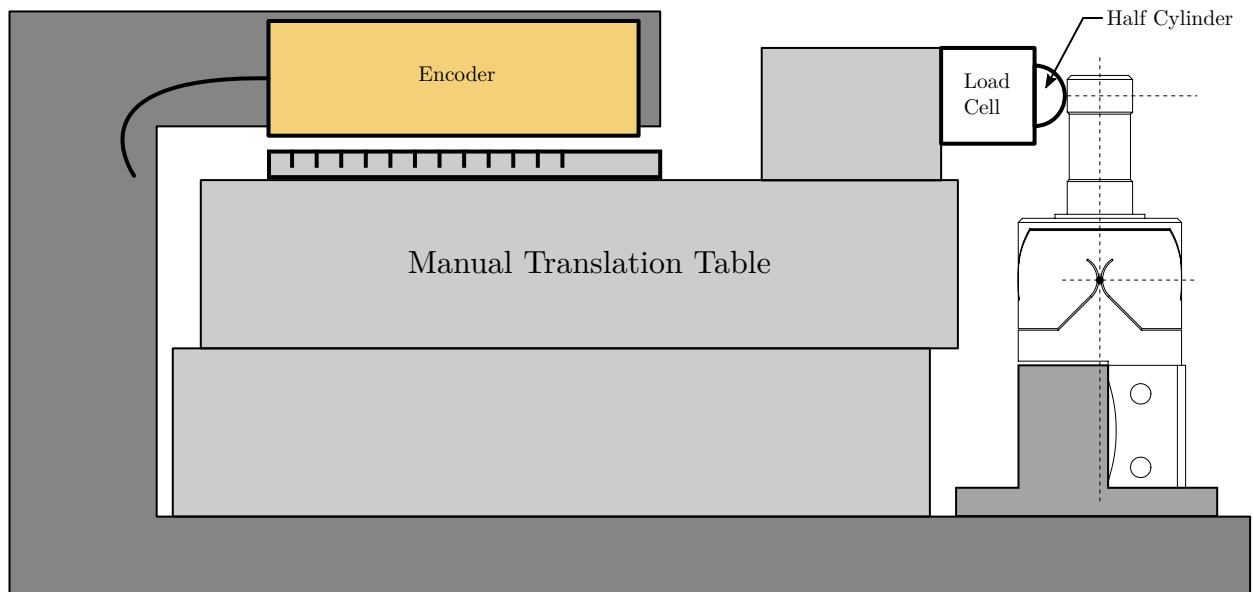
|                   | <b>Specification</b> |
|-------------------|----------------------|
| Axial Stiffness   | $> 200$ [N/um]       |
| Shear Stiffness   | $> 1$ [N/um]         |
| Bending Stiffness | $< 100$ [Nm/rad]     |
| Torsion Stiffness | $< 500$ [Nm/rad]     |
| Bending Stroke    | $> 1$ [mrad]         |
| Torsion Stroke    | $> 5$ [urad]         |

## 2 Test Bench Description

The main characteristic of the flexible joint that we want to measure is its bending stiffness  $k_{R_x} \approx k_{R_y}$ .

To do so, a test bench is used. Specifications of the test bench to precisely measure the bending stiffness are described in this section.

The basic idea is to measure the angular deflection of the flexible joint as a function of the applied torque.



**Figure 2.1:** Schematic of the test bench to measure the bending stiffness of the flexible joints

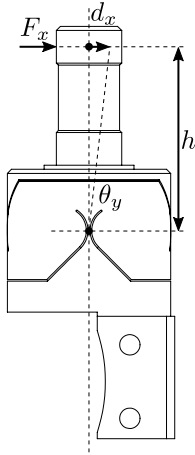
### 2.1 Flexible joint Geometry

The flexible joint used for the Nano-Hexapod is shown in Figure 2.2. Its bending stiffness is foreseen to be  $k_{R_y} \approx 20 \frac{Nm}{rad}$  and its stroke  $\theta_{y,max} \approx 20 mrad$ .

The height between the flexible point (center of the joint) and the point where external forces are applied is  $h = 20 mm$ .

Let's define the parameters on Matlab.

```
Matlab
kRx = 20; % Bending Stiffness [Nm/rad]
Rxmax = 20e-3; % Bending Stroke [rad]
h = 20e-3; % Height [m]
```



**Figure 2.2:** Geometry of the flexible joint

## 2.2 Required external applied force

The bending  $\theta_y$  of the flexible joint due to the force  $F_x$  is:

$$\theta_y = \frac{M_y}{k_{R_y}} = \frac{F_x h}{k_{R_y}} \quad (2.1)$$

Therefore, the applied force to test the full range of the flexible joint is:

$$F_{x,\max} = \frac{k_{R_y} \theta_{y,\max}}{h} \quad (2.2)$$

```
Fxmax = kRx*Rxmax/h; % Force to induce maximum stroke [N] Matlab
```

And we obtain:

$$F_{max} = 20.0 [N] \quad (2.3)$$

The measurement range of the force sensor should then be higher than 20 N.

## 2.3 Required actuator stroke and sensors range

The flexible joint is designed to allow a bending motion of  $\pm 20 \text{ mrad}$ . The corresponding actuator stroke to impose such motion is:

$$d_{x,\max} = h \tan(R_{x,\max})$$

```
dxmax = h*tan(Rxmax);
```

$$d_{max} = 0.4 [mm] \quad (2.4)$$

In order to test the full range of the flexible joint, the stroke of the actuator should be higher than  $0.4\text{ mm}$ . The measurement range of the displacement sensor should also be higher than  $0.4\text{ mm}$ .

## 2.4 First try with the APA95ML

The APA95ML as a stroke of  $100\ \mu\text{m}$  and the encoder in parallel can easily measure the required stroke.

Suppose the full stroke of the APA can be used to bend the flexible joint (ideal case), the measured force will be:

```
Fxmax = kRx*100e-6/h^2; % Force at maximum stroke [N]
```

$$F_{max} = 5.0 [N] \quad (2.5)$$

And the tested angular range is:

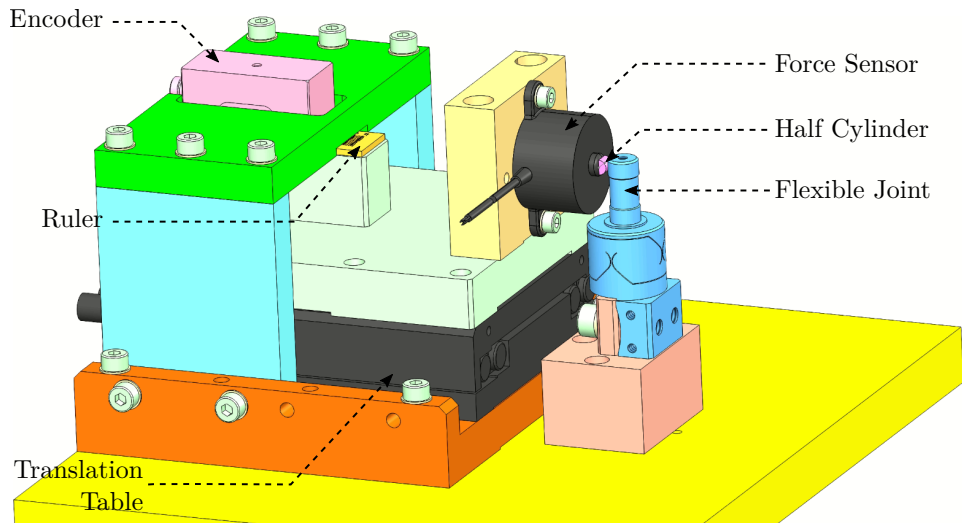
```
Rmax = tan(100e-6/h);
```

$$\theta_{max} = 5.0 [mrad] \quad (2.6)$$

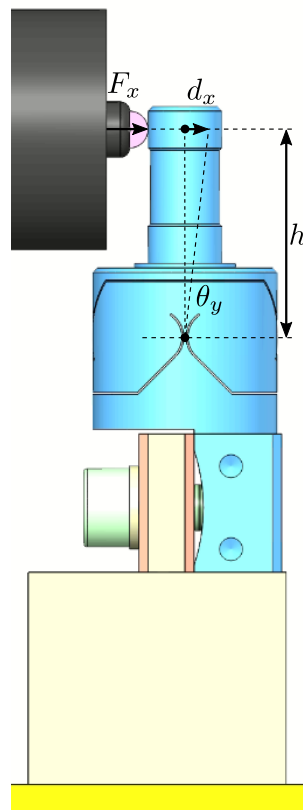
## 2.5 Test Bench

### Note

- **Translation Stage:** V-408
- **Load Cells:** FC2231-0000-0010-L and XFL212R
- **Encoder:** Renishaw Resolute 1nm



**Figure 2.3:** Schematic of the test bench to measure the bending stiffness of the flexible joints



**Figure 2.4:** Schematic of the test bench to measure the bending stiffness of the flexible joints

- **Displacement Probe:** Millimar C1216 electronics and Millimar 1318 probe



# 3 Agreement between the probe and the encoder

## 3.1 Setup

The measurement setup is made such that the probe measured the translation table displacement. It should then measure the same displacement as the encoder. Using this setup, we should be able to compare the probe and the encoder.

## 3.2 Results

Let's load the measurements.

```
load('meas_probe_against_encoder.mat', 't', 'd', 'dp', 'F')
```

The time domain measured displacement by the probe and by the encoder is shown in Figure 3.1.

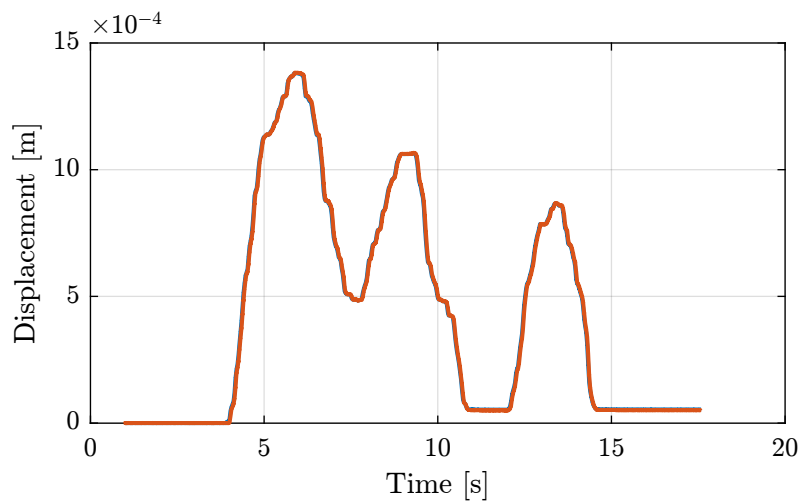
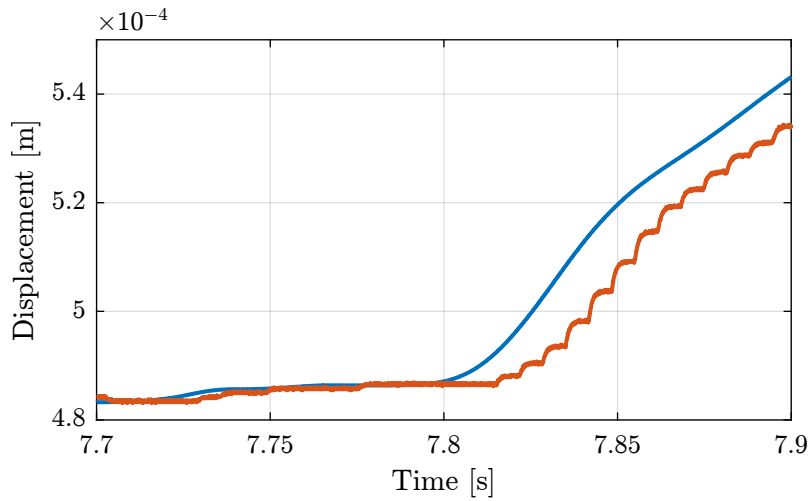


Figure 3.1: Time domain measurement

If we zoom, we see that there is some delay between the encoder and the probe (Figure 3.2).

This delay is estimated using the `finddelay` command.

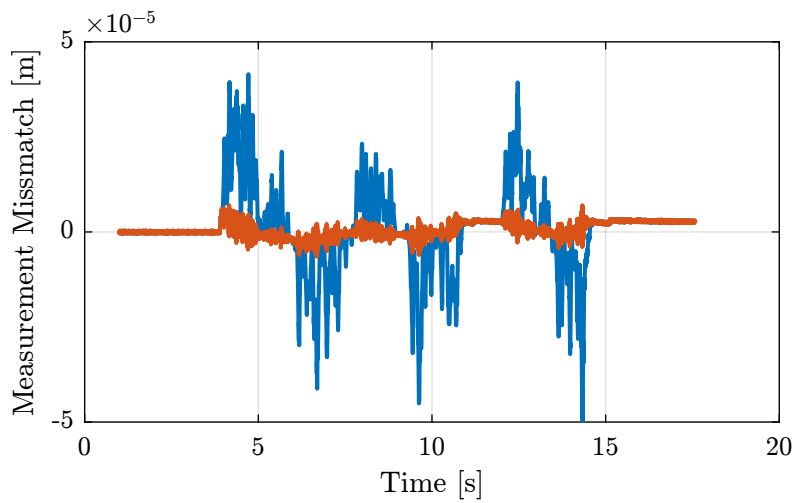


**Figure 3.2:** Time domain measurement (Zoom)

Results

The time delay is approximately 15.8 [ms]

The measured mismatch between the encoder and the probe with and without compensating for the time delay are shown in Figure 3.3.

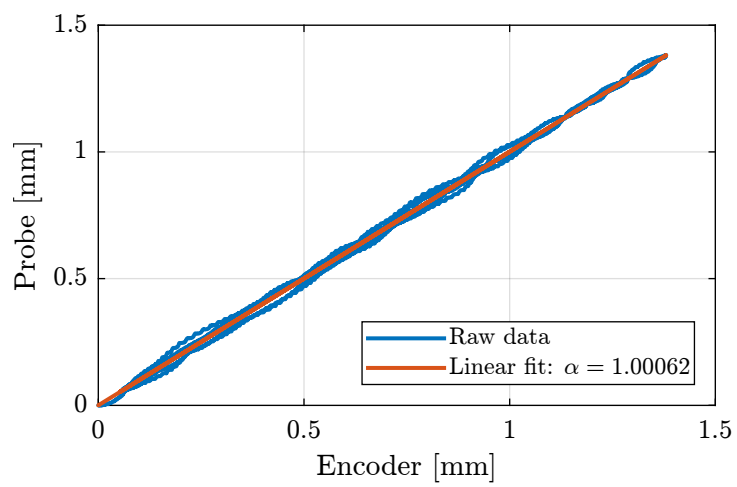


**Figure 3.3:** Measurement mismatch, with and without delay compensation

Finally, the displacement of the probe is shown as a function of the displacement of the encoder and a linear fit is made (Figure 3.4).

**Important**

From the measurement, it is shown that the probe is well calibrated. However, there is some time delay of tens of milliseconds that could induce some measurement errors.



**Figure 3.4:** Measured displacement by the probe as a function of the measured displacement by the encoder

## 4 Measurement of the Millimar 1318 probe stiffness

### Note

- Translation Stage: V-408
- Load Cell: FC2231-0000-0010-L
- Encoder: Renishaw Resolute 1nm
- Displacement Probe: Millimar C1216 electronics and Millimar 1318 probe

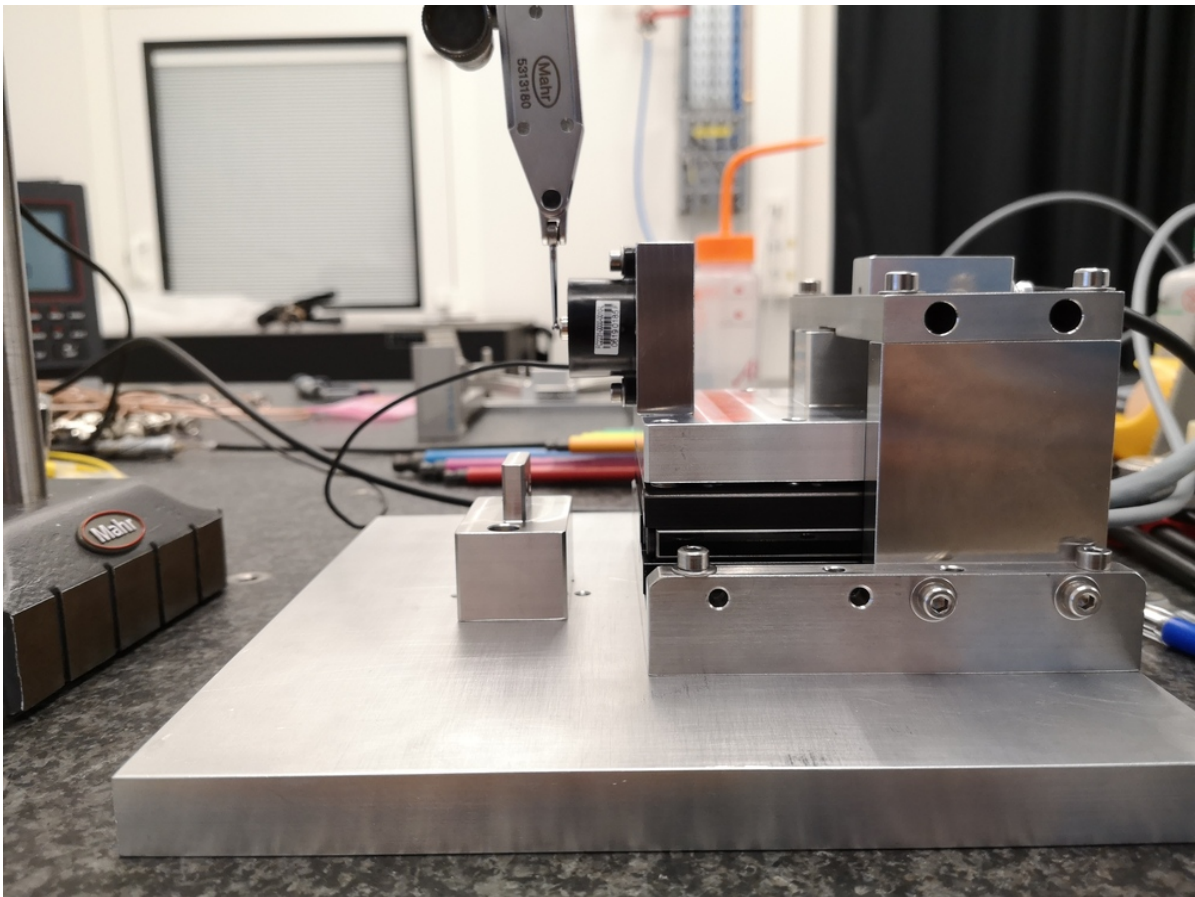


Figure 4.1: Setup - Side View

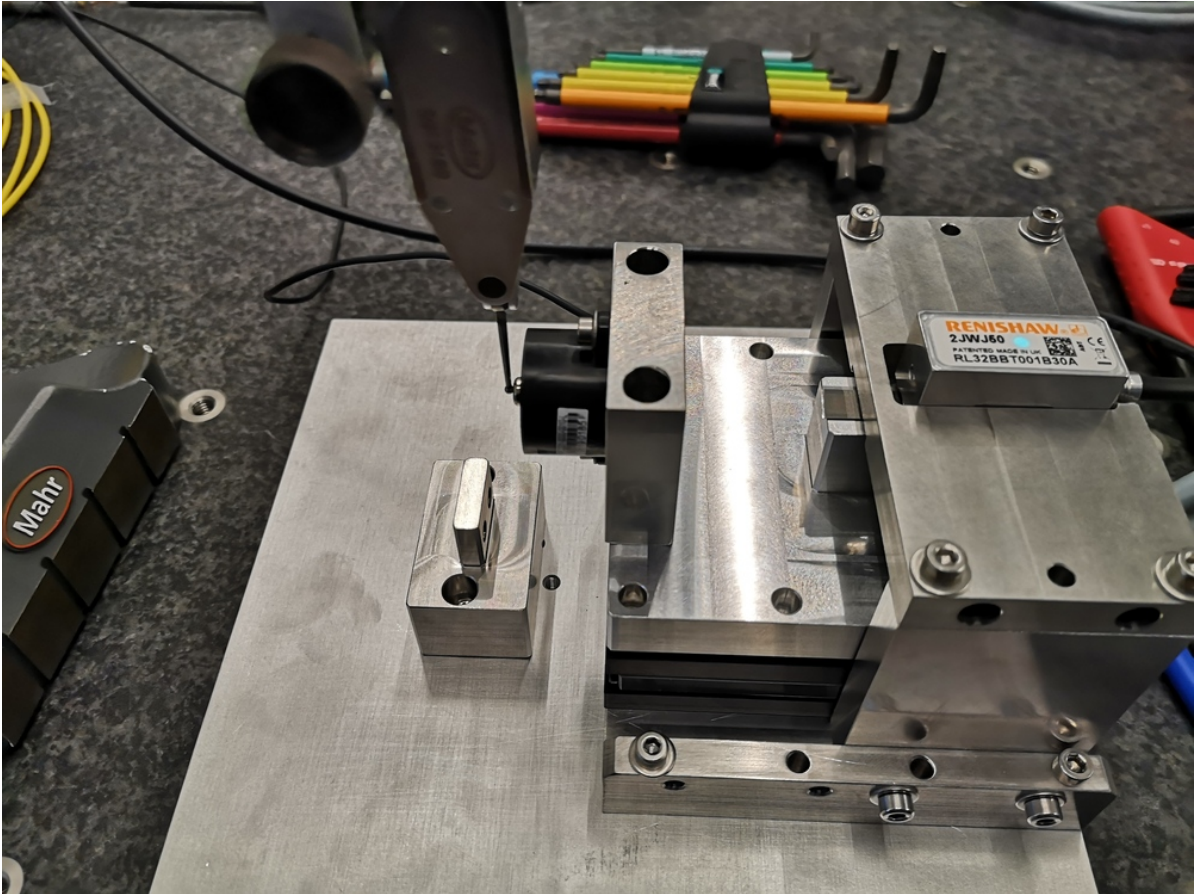


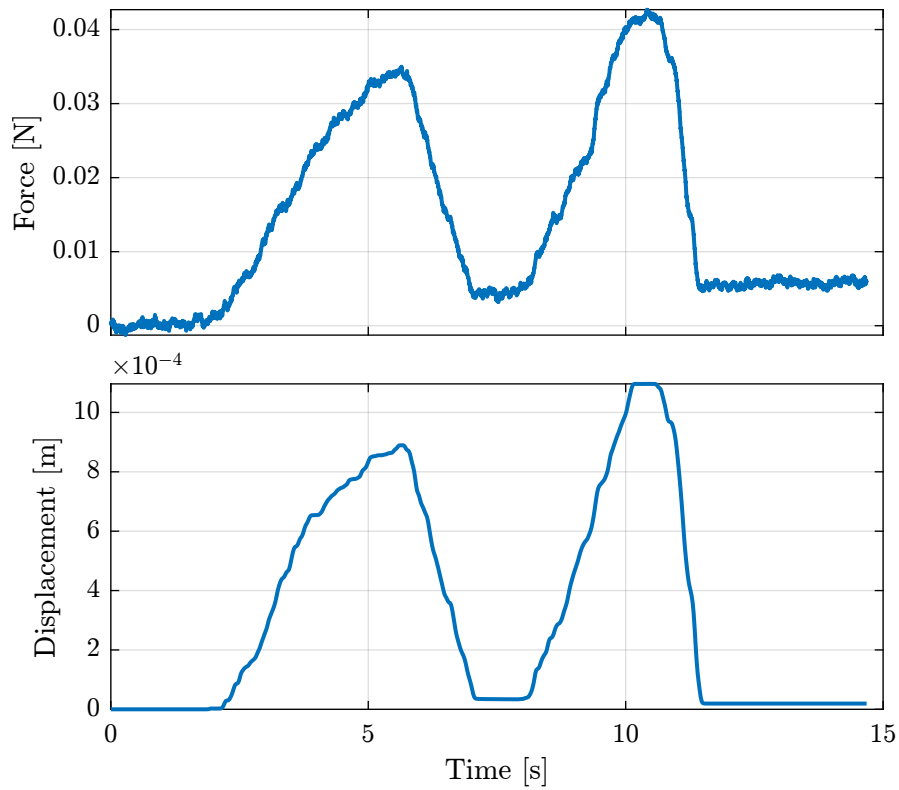
Figure 4.2: Setup - Top View

## 4.1 Results

Let's load the measurement results.

```
load('meas_stiff_probe.mat', 't', 'd', 'dp', 'F')
```

The time domain measured force and displacement are shown in Figure 4.3.



**Figure 4.3:** Time domain measurements

Now we can estimate the stiffness with a linear fit.

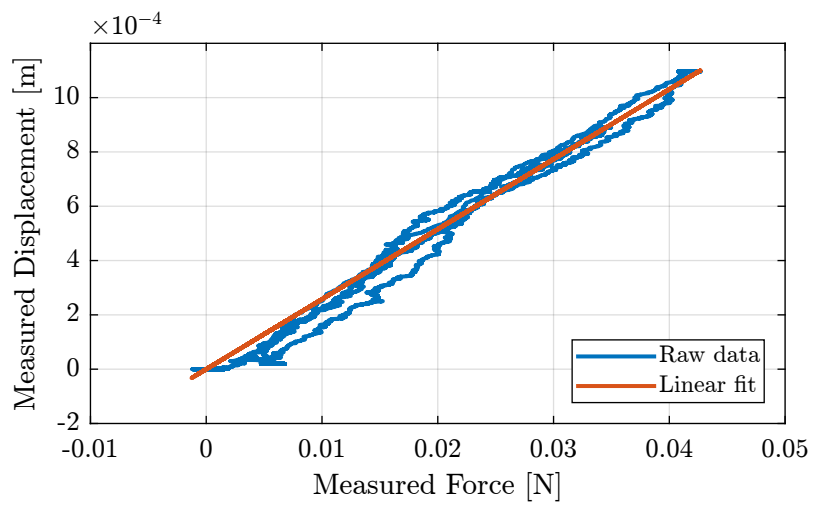
```
Stiffness is 0.039 [N/mm]
```

This is very close to the 0.04 [N/mm] written in the [Millimar 1318 probe datasheet](#).

And compare the linear fit with the raw measurement data (Figure 4.4).

### Summary

The Millimar 1318 probe has a stiffness of  $\approx 0.04$  [N/mm].



**Figure 4.4:** Measured displacement as a function of the measured force. Raw data and linear fit

## 5 Experimental measurement