

Active Damping of Rotating Platforms using Integral Force Feedback

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Outline

Dynamics of Rotating Platforms

Decentralized Integral Force Feedback

Integral Force Feedback with High Pass Filter

Integral Force Feedback with Parallel Springs

Comparison and Discussion

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Model of a Rotating Positioning Platform

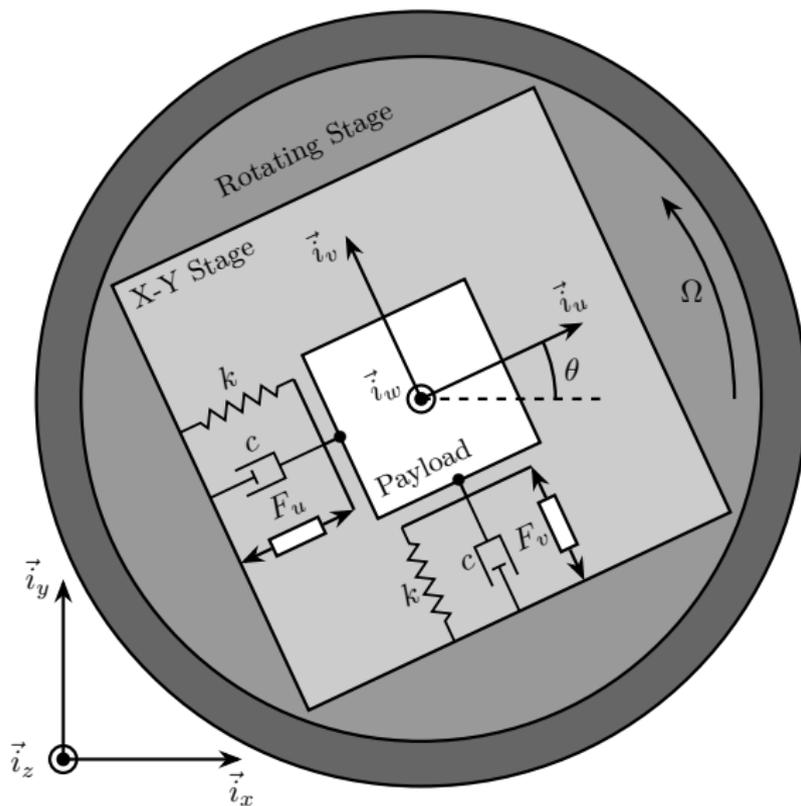


Fig.: Schematic of the studied System

Equations of Motion - Lagrangian Formalism

Lagrangian equations:

$$\frac{d}{dt} \left(\frac{\partial L}{\partial \dot{q}_i} \right) + \frac{\partial D}{\partial \dot{q}_i} - \frac{\partial L}{\partial q_i} = Q_i$$

Equations of motion:

$$\begin{aligned} m\ddot{d}_u + c\dot{d}_u + (k - m\Omega^2)d_u &= F_u + 2m\Omega\dot{d}_v \\ m\ddot{d}_v + c\dot{d}_v + \underbrace{(k - m\Omega^2)}_{\text{Centrif.}}d_v &= F_v - \underbrace{2m\Omega\dot{d}_u}_{\text{Coriolis}} \end{aligned}$$

Centrifugal forces \iff Negative Stiffness
Coriolis Forces \iff Coupling

Transfer Function Matrix the Laplace domain

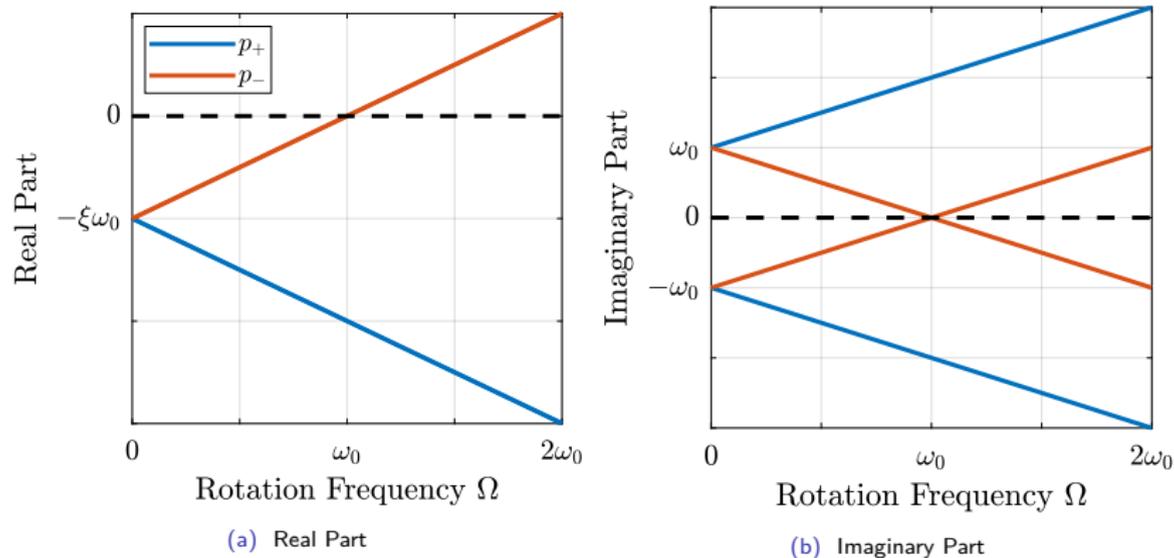


Fig.: Campbell Diagram : Evolution of the complex and real parts of the system's poles as a function of the rotational speed Ω

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Force Sensors and Decentralized IFF Control Architecture

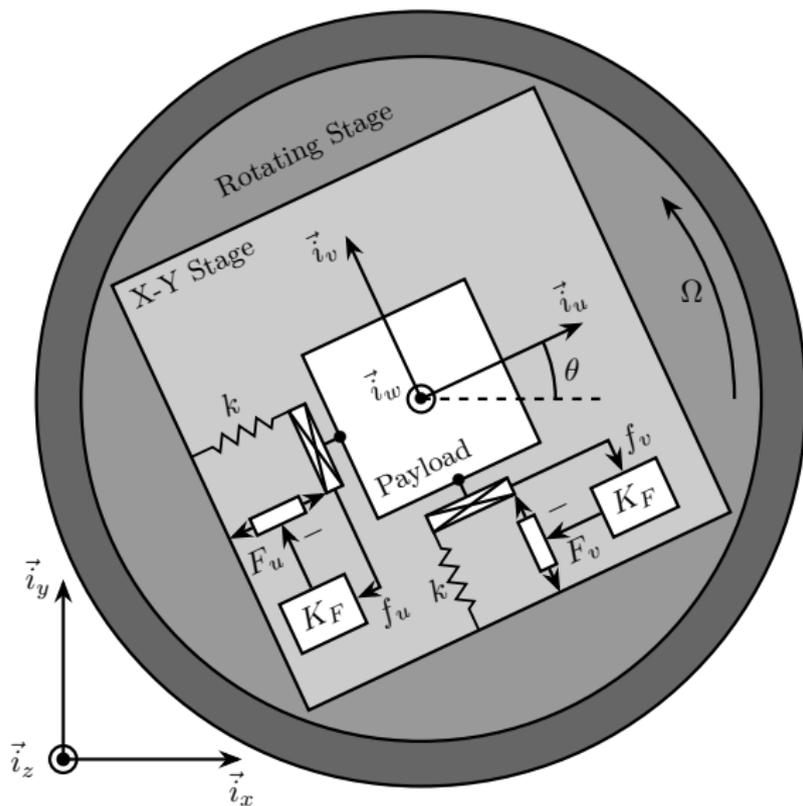


Fig.: System with added Force Sensor in series with the actuators, $K_F(s) = g \cdot \frac{1}{s}$

IFF Plant Dynamics

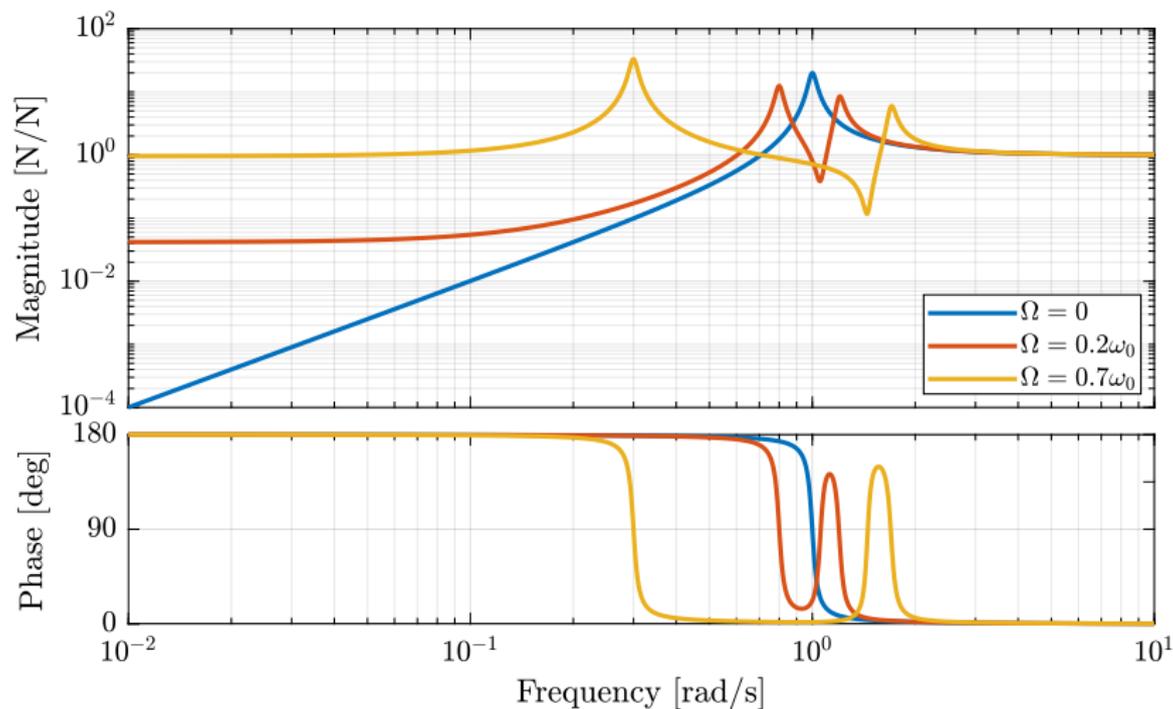


Fig.: Bode plot of the dynamics from force actuator to force sensor for several rotational speeds Ω

Decentralized IFF with Pure Integrators

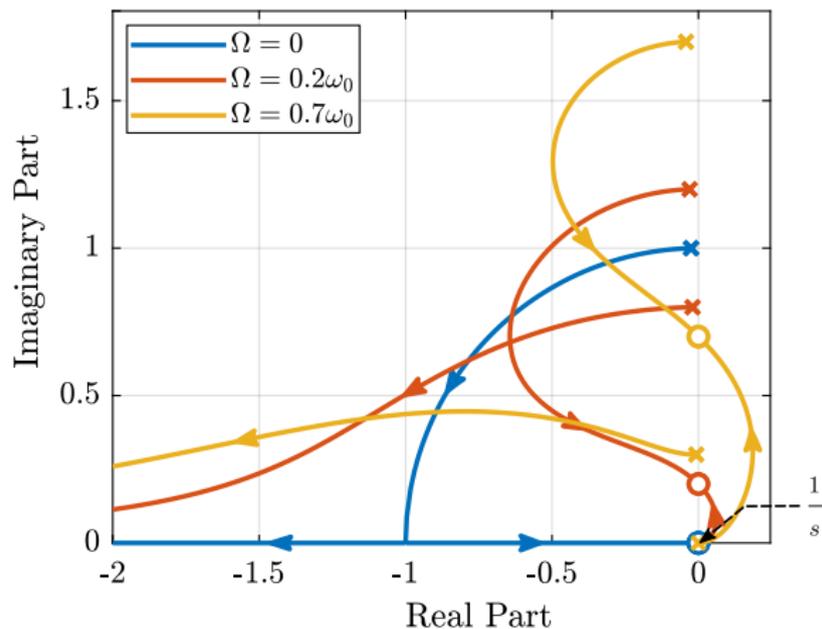


Fig.: Root Locus for Decentralized IFF for several rotating speeds Ω

For $\Omega > 0$, the closed loop system is unstable

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Modification of the Control Law

$$K_F(s) = g \cdot \frac{1}{s} \cdot \underbrace{\frac{s/\omega_i}{1 + s/\omega_i}}_{\text{HPF}} = g \cdot \frac{1}{s + \omega_i}$$

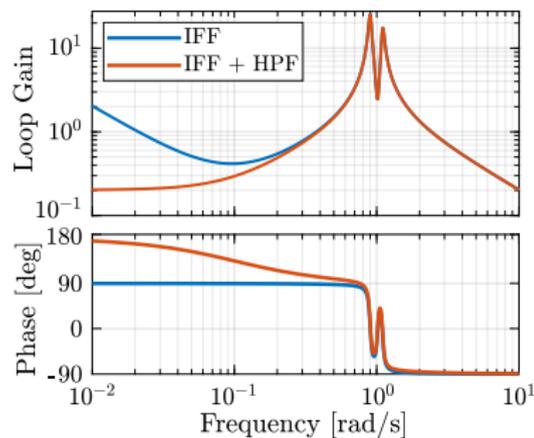


Fig.: Loop Gain

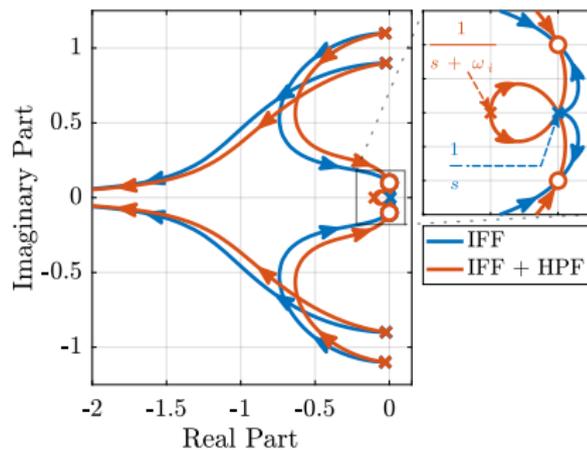


Fig.: Root Locus

Effect of ω_i on the attainable damping

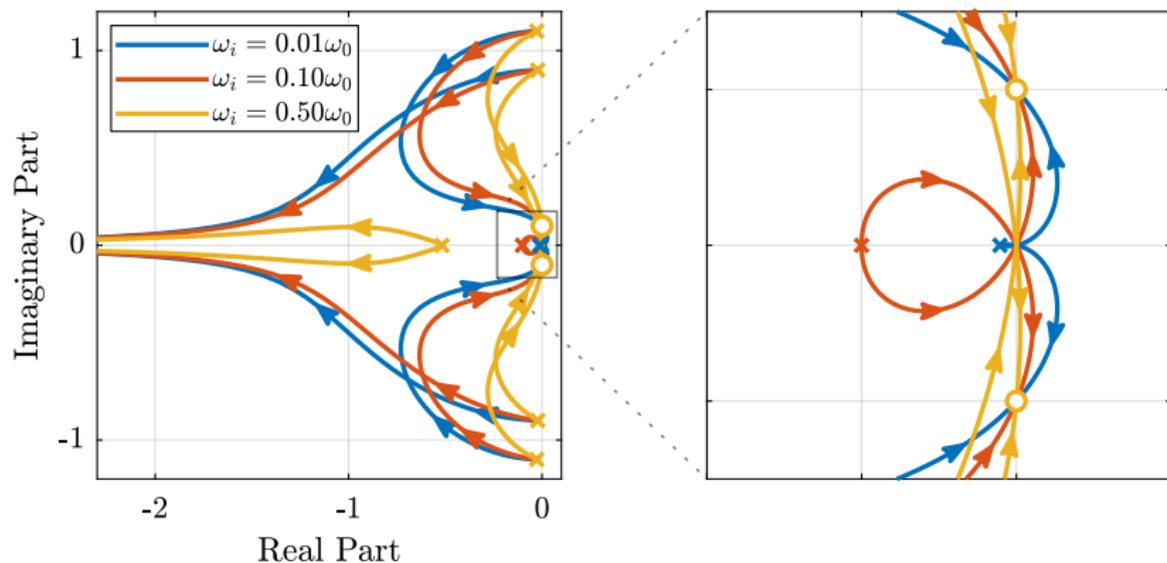


Fig.: Root Locus for several HPF cut-off frequencies ω_i , $\Omega = 0.1\omega_0$

$$g_{\max} = \omega_i \left(\frac{\omega_0^2}{\Omega^2} - 1 \right)$$

small $\omega_i \implies$ increase maximum damping
small $\omega_i \implies$ reduces maximum gain g_{\max}

Optimal Control Parameters

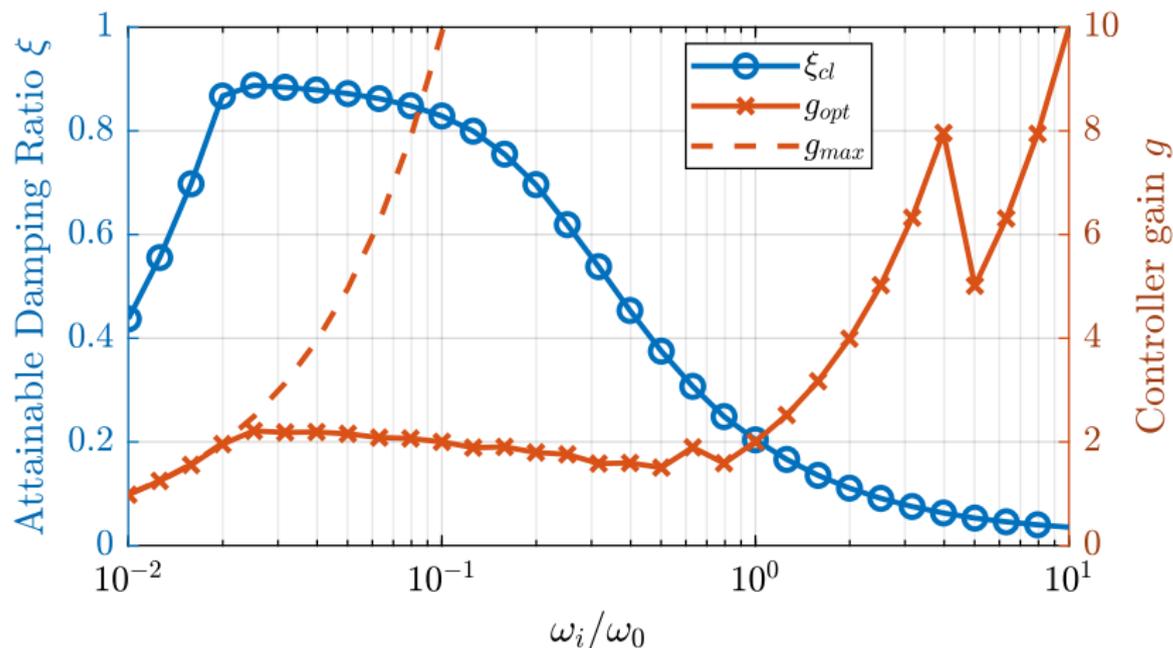


Fig.: Attainable damping ratio ξ_{cl} as a function of the ratio ω_i/ω_0 . Corresponding control gain g_{opt} and g_{max} are also shown

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Stiffness in Parallel with the Force Sensor

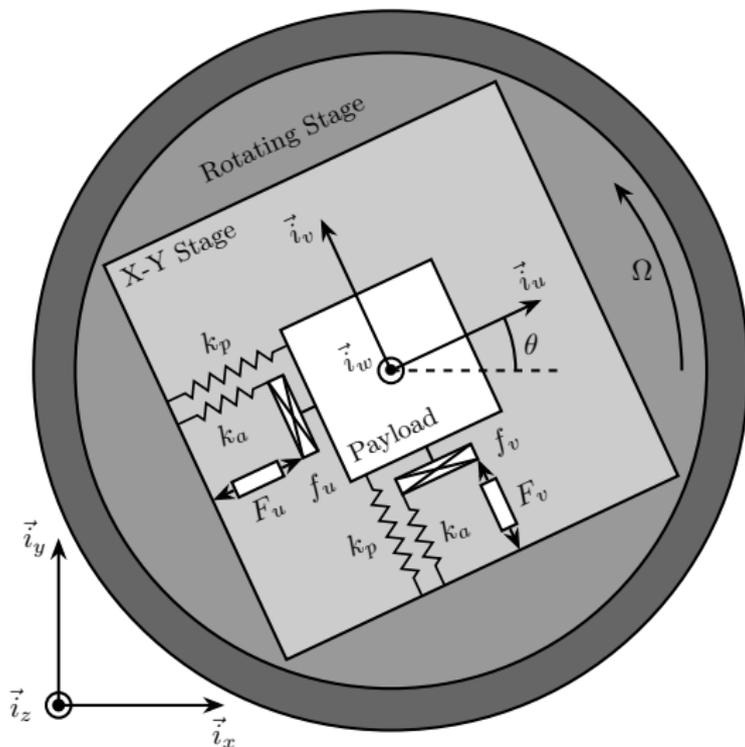


Fig.: System with additional springs in parallel with the actuators and force sensors

Effect of the Parallel Stiffness on the Plant Dynamics

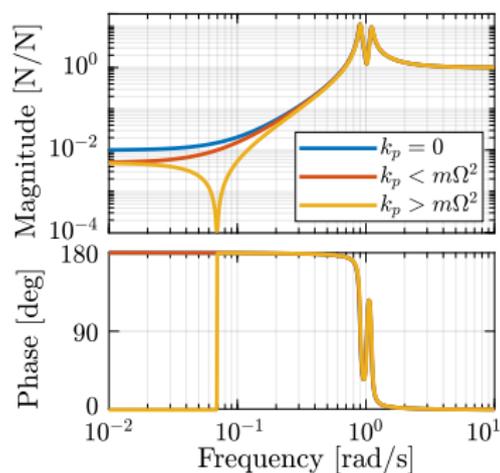


Fig.: Bode Plot of f_u/F_u

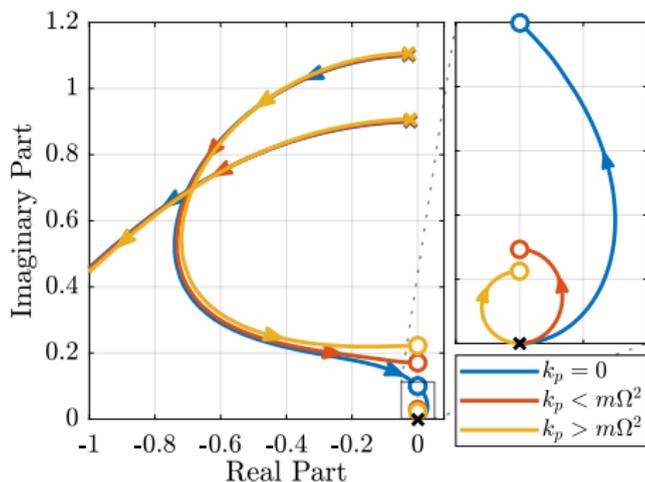


Fig.: Root Locus for IFF

If $k_p > m\Omega^2$, the poles of the closed-loop system stay in the (stable) right half-plane, and hence the **unconditional stability of IFF is recovered**.

Optimal Parallel Stiffness

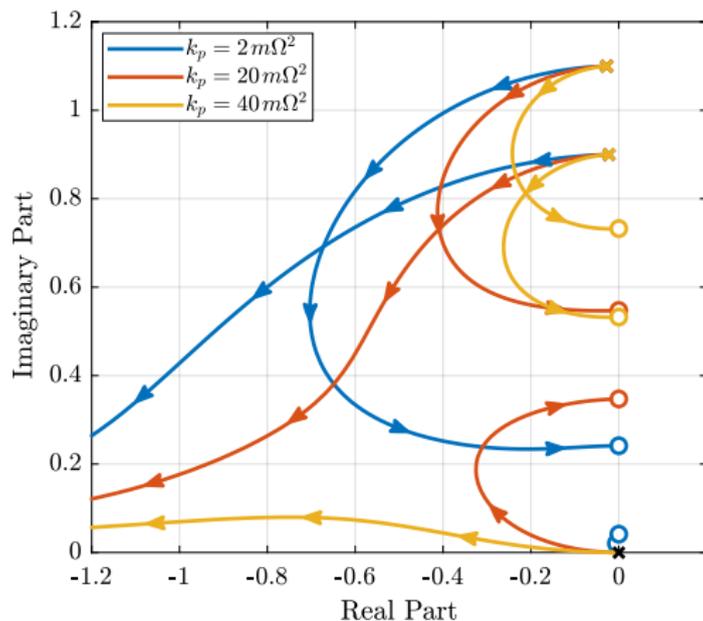


Fig.: Root Locus for three parallel stiffnesses k_p

Large parallel stiffness k_p reduces the attainable damping.

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Comparison of the Attainable Damping

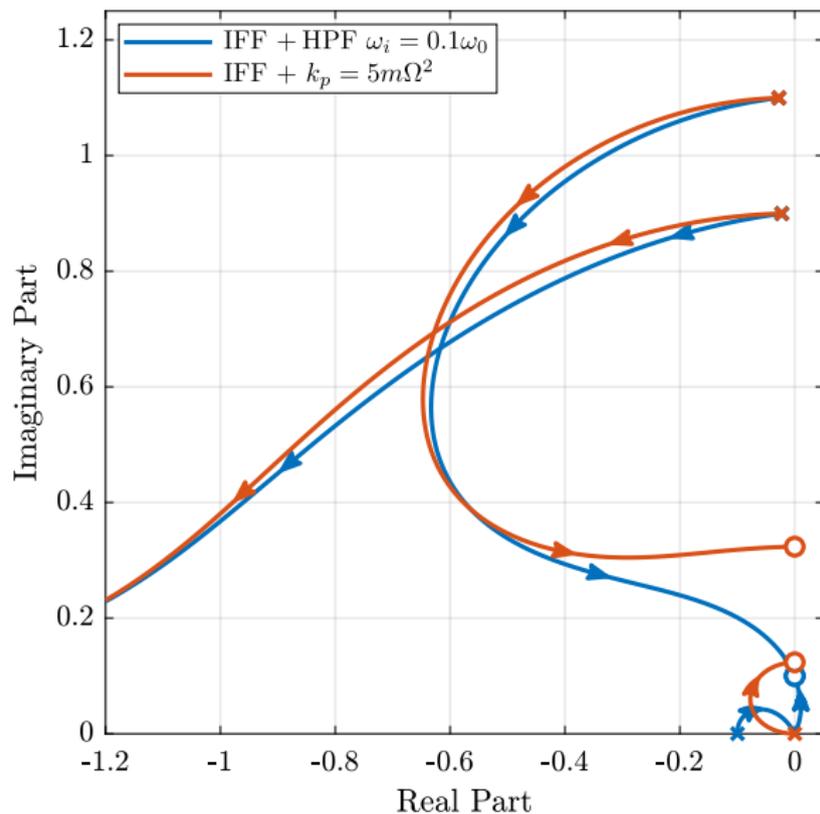
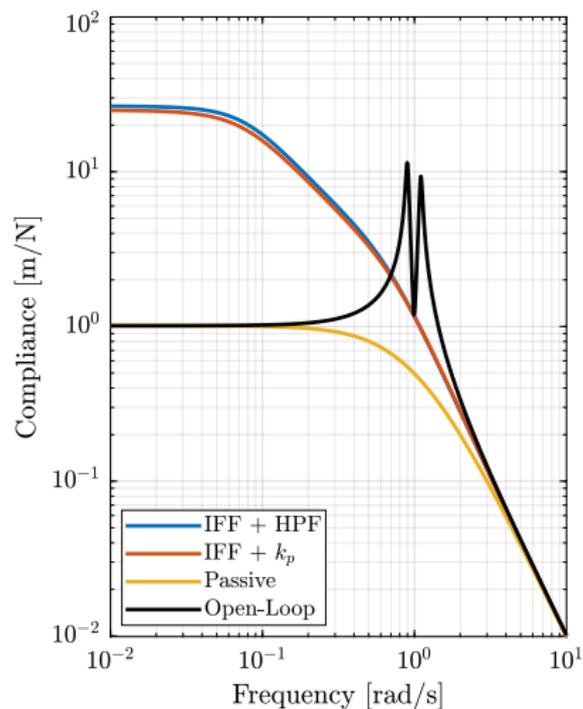
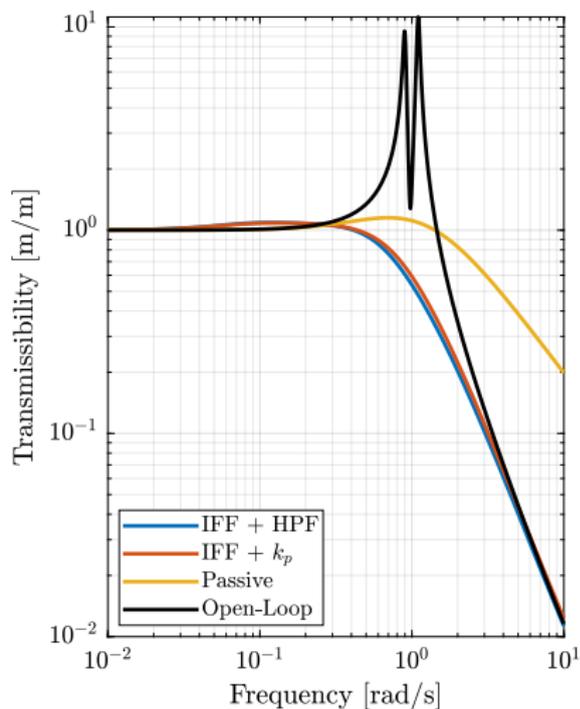


Fig.: Root Locus for the two proposed modifications of decentralized IFF, $\Omega = 0.1\omega_0$

Comparison Transmissibility and Compliance



(a) Compliance



(b) Transmissibility

Fig.: Comparison of the two proposed Active Damping Techniques, $\Omega = 0.1\omega_0$

Thank you!

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https://tdehaeze.github.io/dehaeze20_contr_stewa_platf/